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Europäisches Patentamt

European Patent Office

Office européen des brevets

⑪

Publication number:

**0 230 212
A2**

⑫

EUROPEAN PATENT APPLICATION

⑲ Application number: 86830382.7

⑤① Int. Cl. 4: **C08L 23/02** , **C08L 23/16** ,
//(C08L23/02,23:16)

⑳ Date of filing: 18.12.86

③① Priority: 20.12.85 IT 365685

④③ Date of publication of application:
29.07.87 Bulletin 87/31

⑥④ Designated Contracting States:
AT BE CH DE ES FR GB GR LI NL SE

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⑤④ A process for the preparation of plastomer-elastomer compounds from polyolefins and EPDM terpolymers, and plastomer-elastomer compounds obtained with such a process.

⑤⑦ The process permits of obtaining plastomer-elastomer compounds from olefinic thermoplastic resins and EPDM elastomers, in which cross-linking of the elastomer phase may occur either wholly or in part; conventional thermodynamic vulcanizing methods are employed, and a non-halogenated phenolic resin is used in conjunction with an aromatic carboxylic acid to bring about cross-linking.

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A process for the preparation of plastomer-elastomer compounds from polyolefins and EPDM terpolymers, and plastomer-elastomer compounds obtained with such a process.

The invention disclosed relates to a process for the preparation of plastomer-elastomer compounds from thermoplastic olefin resins and ethylene propylene terpolymers, and to plastomer-elastomer compounds obtained by implementation of such a process. The preparation of thermoplastics from α -olefin resins and EPDM terpolymeric elastomers has long constituted prior art in the field in question, e.g. as in
 5 FR 2 408 632 published 1978, and US 849 773 published 1977. In the preparation methods disclosed by these two references, the cross-linking agent employed is either a halogenated phenolic resin, or a non-halogenated phenolic resin associated with halogen donors.

US 4 477 631, published in 1984, discloses the association of a non-halogenated phenolic resin with metal oxides or carbonates; processability is thus enhanced in comparison to the two references first
 10 mentioned.

Other elastomer vulcanizing techniques that fall within the general scope of preparing plastomer-elastomer compounds from α -olefin plastomers and EPDM elastomers, thermodynamically cross-linked, are described in DE 2 401 149, published 1974, also in US 322 360, and US 3 884 882, published 1973 and '74 respectively, which disclose initial bonding of the elastomeric copolymers with maleic anhydride so as to
 15 ensure their being cross-linked and rendered more compatible with the plastomer materials contained in the compounds.

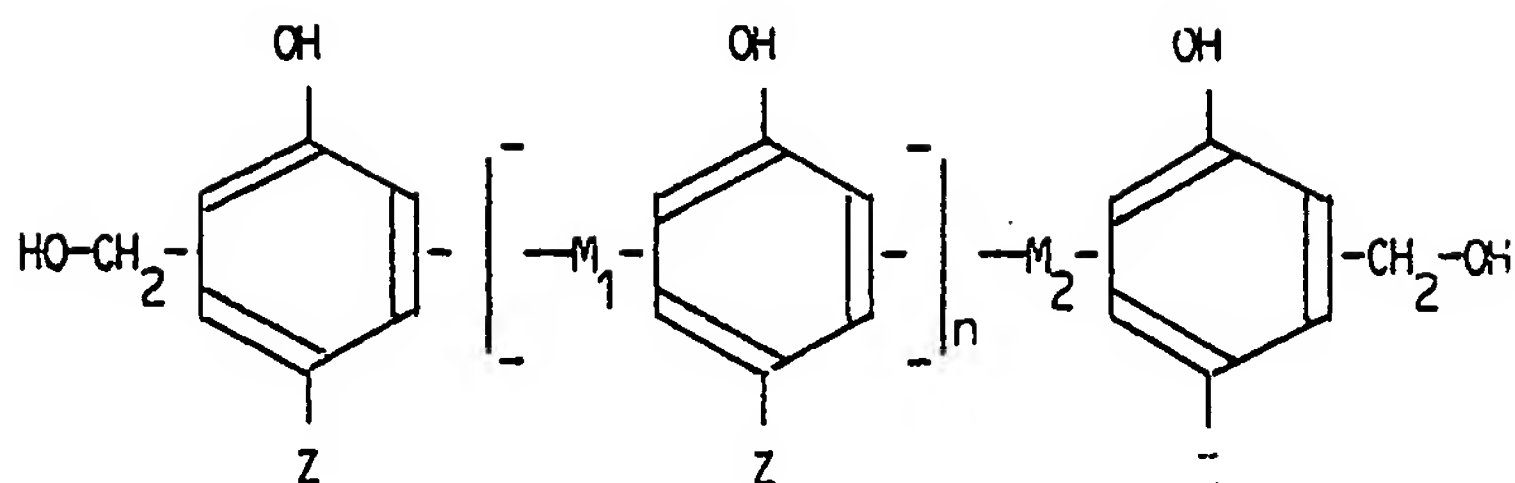
Finally, the prior art also embraces methods for the preparation of plastomer-elastomer compounds wherein the elastomeric constituent is cross-linked thermodynamically employing conventional agents such as are used in the rubber industry, namely, sulphur or its donors, organic peroxides, quinone derivatives, guanidine, azides, sulphenazides, amines, xanthates, urea, triazoles, imidazoles, sulphenamides, cyanide
 20 compounds, isocyanates, and paraquinondioxin (as disclosed in GB 2 011 430, published 1978, also in US 3 806 558 and US 3 037 954, both published 1973, and US 3 758 643 and 3 862 106, both published 1974. There are drawbacks common to all the thermodynamic vulcanization methods embraced by the prior art, the effect of which is to impose marked limitations on the use of the compound, and/or on the possibility of its being manufactured with ease. For example, cross-linking of the rubbery component (EPDM) is uneven by reason of the poor dispersion of cross-linking agents within the given plastomer-elastomer compound as a whole, once temperature levels equal to or higher than that of the plastomer's melting point are reached, as vulcanization of the elastomer content commences at temperatures of this order. Other processes protected by letters patent tend to disclose over-long reaction times and excessively high temperatures,
 25 which are not practicable at industrial level.

Accordingly, the object of the invention is that of setting forth a new process that improves on prior art methods, inasmuch as the plastomer-elastomer compound is more easily processed, and operating conditions are engineered in a way such as enhances feasibility of the process on industrial scale. More exactly, the object is one of developing a process that will be ensured free from the drawbacks mentioned
 35 above, especially in terms of avoiding environmental and personal risk stemming from the production of chlorine, and require considerably lower temperatures and less time for implementation than the processes employed hitherto.

The stated object can be realized to surprisingly good effect, using a non-halogenated phenolic resin in conjunction with a given aromatic carboxylic acid to bring about thermodynamic cross-linking of the EPDM elastomeric content present in the plastomer-elastomer compound.
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A process according to the invention, serving for the preparation of plastomer-elastomer compounds from EPDM terpolymers and polyolefin resins, wherein the elastomer phase is part or totally cross-linked, is characterized in that the cross-linking agent adopted takes the form of a non-halogenated phenolic resin and an aromatic carboxylic acid, utilized in conjunction.

45 More exactly, the cross-linking non-halogenated phenolic resin is an alkylphenol-formaldehyde resin having the general formula:



where

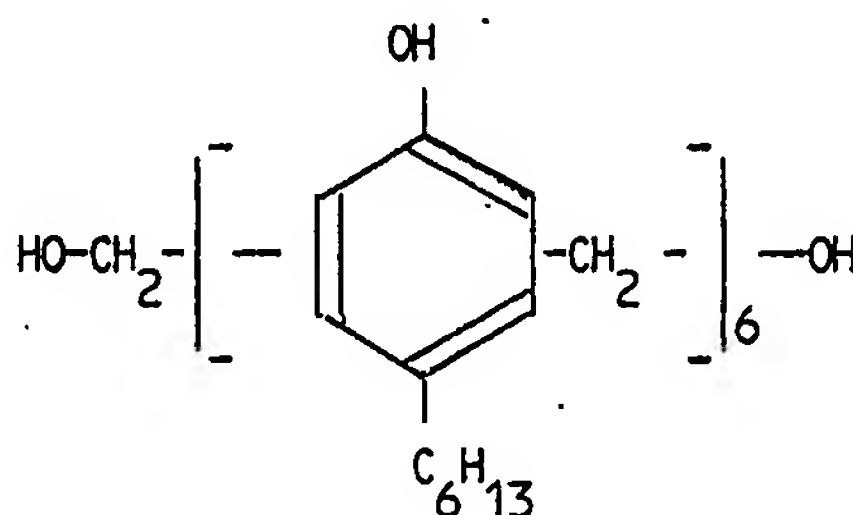
M₁ and M₂ are radicals -CH₂- or -CH₂-C(=O)-CH₂-,

which can be identical or otherwise;

Z is an alkylenic, aryllic or alkylic radical having from 4 to 16 carbon atoms;

n is an integer between 0 and 6.

In a preferred version of the process, the phenolic resin will be a phenol-formaldehyde type resol with the following written formula:



To achieve cross-linking, the non-halogenated phenolic resin must be utilized together with an aromatic carboxylic acid, and according to the invention, salicylic acid has proved especially suitable to the purpose - viz,

chemical formula: $\text{HO-C}_6\text{H}_4\text{-} \begin{array}{c} \text{C} = \text{O} \\ | \\ \text{O H} \end{array}$

molecular weight: 138.12

melting point: 159 °C

specific weight: 1.37 g/cc

The vulcanizing method adopted according to the invention thus consists in the combination of an alkylphenol-formaldehyde resin, preferably phenol-formaldehyde resol, with salicylic acid, wherein 0.1...0.8 parts acid are admixed, by weight, to each part resin.

The process for preparation of plastomer-elastomer compounds consists, according to the invention, in using equipment of the conventional type employed in plastics and/or rubber manufacture, namely Banbury mixers, compounding augers, Buss mixers &c. to work up mixtures containing 10...80% by weight of EPDM terpolymer (at least two α-olefin monomers and at least one diene monomer), and a cross-linking agent consisting in 0.5...15 parts by weight per 100 parts EPDM of a non-halogenated phenolic resin to which salicylic acid is admixed at a rate of between 0.1 and 0.8 parts per 1 part resin, likewise by weight. The reaction occurs at a temperature equal to or higher (preferably higher) than that of the melting point of the olefin thermoplastic employed, and for a duration sufficient to ensure a thorough mix, and partial or total (preferably total) cross-linking of the rubbery EPDM.

The operation can be effected in any single one of the compounding machines described above, or using a train of machines (e.g. Banbury mixer-+-extruder, dry turbo mixer-+-twin-auger extruder, or Banbury-+-Buss &c...). Whatever the ultimate choice of plant, the process must be implemented dynamically, with duration, temperature and rotational speed of the machine such as will ensure the following sequence of steps:

- mastication of the EPDM elastomer and fusion of the polyolefin plastomer;
- thorough dispersion of the components;
- cross-linking of the elastomeric component;
- even dispersion of any other additives.

Proceeding thus, it becomes possible to obtain a fine dispersion of the cross-linked EPDM elastomer - (indiscrete phase), merged with the molten plastomer (discrete phase) and assuming the form of minute nodular particles measuring some 0.1...1.5 μm in diameter.

The ideal process temperature would be of an order of 160...240 °C, whereas the mastication time lapse will depend upon:

- a) the degree of EPDM elastomer cross-linking it is wished to achieve;
- b) the proportion of diene, by weight, in the EPDM polymer chain;
- c) the proportion, by weight, of the cross-linking agents employed (phenolic resin + salicylic acid).

The following observations must also be made with regard to the single components:

1) the EPDM should be linked at a rate of between 10 and 100% by weight of the total amount incorporated into the compound; the ideal proportion is 58...98%, by weight;

2) the proportion of diene in the EPDM, a parameter which is determined by the degree of unsaturation and generally expressed as parts diene per 100 parts elastomer (by weight), can vary between 1 and 15%; the process will be best implemented utilizing EPDM elastomers containing between 3 and 8% diene, by weight;

3) the quantities by weight of dynamic cross-linking agent to be admixed to the EPDM elastomer should be between 0.5 and 15 parts phenolic resin, and between 0.05 and 12 parts salicylic acid.

A thermodynamically cross-linked plastomer-elastomer mix according to the invention may include additives of the types used conventionally for such compounds -viz, strengtheners, whether organic (carbon black) or inorganic (silica and silicates), plasticizers (mineral oils, wax, paraffin), fillers (carbonates, kaolin, talc, calcined clay, heavy spar, asbestos and the like), antioxidants, ozone and ultra-violet inhibitors, peptizing agents and anticoagulants, organic and inorganic pigments, vulcanizing agents. All of the components employed in formulation of a given plastomer-elastomer compound according to the invention are either conventional substances, or substances which can be prepared using processes embraced by the prior art. The following definitions are given by way of example.

EPDM terpolymers, as envisaged in the terms of the invention, are prevalently amorphous polymers which consist of ethylene, with at least one α -olefin (propylene or 1-butene) and at least one diene that may be linked with the principal polymer chain or otherwise, and consists of the following monomers: ethylidene-norbornene, 1,4-hexadiene, dicyclopentadiene, 2-methyl-1,4-pentadiene, 1,4,9-decatriene, 1,5-cyclooctadiene, 1-methyl-1,5-cyclooctadiene, 1,4-cyclopentadiene, polybutene, polybutadiene, and their substitute derivatives.

Such terpolymers have molecular weight of between 50,000 and 800,000, an ethylene content of between 20 and 80% mol., and bonded diene content of between 1 and 15 parts per 100 parts polymer, by weight; the remainder will consist of an α -olefin, which may be propylene or butylene.

Olefin plastomers, likewise within the scope of the invention, are olefin copolymers obtained by the interreaction of olefinic monomers such as ethylene, propylene, 1-butene, 1-pentene, 1-hexene, 4-methyl-1-pentene, 3-methyl-1-pentene, 3,3-dimethyl-1-butene 3-methyl-1-hexene and 2,4,4-trimethyl-1-pentene. The copolymerization of homogeneous or non-homogeneous monomers ('random' copolymers) is brought about in the presence of metallic/organic catalyst compounds (e.g. $-\text{AlEt}_3$, AlEt_2Cl , Al is Bu_3) together with soluble vanadium compounds (e.g. VCl_3 , VOCl_3 , VACl_3), where Et = ethylene, AC = acetylacetone, and is Bu = isobutyl).

Phenolic resins, i.e. as represented by the general formula given above, are those which can be prepared by condensation of alkyl-phenols with formaldehyde, for example as described in volume 2 of Kunststoffe, pp19...21 (published 1962).

Plastomer-elastomer compounds obtainable by way of the process disclosed would be used in a number of industrial applications, for example:

a) rigid plastic items manufactured using injection, transfer, compression and blow moulding techniques;

b) extruded items, including sheaths for electrical wires and cable;

c) laminated, or 'sheet' material turned out by two or more mill rolls and utilized generally for damp- and weatherproofing;

d) modification of other materials by addition of appropriate percentage quantities of the compounds disclosed herein.

Additives might be formulated for the purpose of enhancing the processability and/or properties of materials such as olefin plastomers, natural and synthetic elastomers, bitumen, asphalts, lubricating oils, adhesives, and polyamine polymers.

Compounds according to the invention can also be utilized dissolved in organic solvents, in any given proportions by weight, for the treatment of natural and/or synthetic fibre fabrics, metal and timber surfaces, cellulose compositions, non-woven fabrics and cement mortar.

The three examples listed below are illustrative of compounds obtainable by implementation of a process as disclosed, though it will be appreciated that no limitation of the basic concept is implied.

Example 1

Plastomer-elastomer compounds are prepared in a Banbury mixer of 6 litres fluid capacity (rotor speed 45 rpm), utilizing components of the type and in the proportions by weight indicated in table 1 (tests A, B, C, D and E).

The EPDM elastomer is put in first and masticated for 30 seconds at an initial temperature of 160 °C, whereupon the polypropylene plastomer and paraffin oil plasticizer are added. Mastication is continued until the rubbery phase is brought about, with complete fusion of the polypropylene, hence its full and even dispersion. This operation requires some two minutes, during which time the temperature in the mixer will rise to 190 °C as a result of the shear strain and friction generated. Next follows admixture of the cross-linking agents, resol and salicylic acid. The components are now masticated further (5 minutes approx) until the EPDM has been fully cross-linked; temperature of the material as it emerges from the machine will be 200 °C approx. In addition to the mix proportions, table 1 shows physical and mechanical properties of the compounds produced, and the essential physical and structural composition of the plastomers, the elastomers and the plasticizers envisaged in this first example. Also listed are the ASTM methods adopted for tests on physical and mechanical properties.

TABLE 1

INGREDIENTS	Quantities expressed as parts per 100 parts EPDM				
	A	B	C	D	E
EPDM	100	100	100	100	100
Polypropylene	80	100	120	150	200
Paraffin oil	100	90	80	100	120
Phenolic resin - resol	10	10	10	10	11
Salicylic acid	3	3	3	3	3.2
Physical and mechanical properties of compounds measured on specimens punched from injection molded slabs					
	A	B	C	D	E
U.T.S. kg/cm^2	90	110	150	180	210
Elongation at U.T.S. %	300	345	500	540	590
Shore hardness A pts	57	85	88	-	-
Shore hardness D pts	-	-	-	35	45
Proportion of total EPDM content cross- linked (by weight) %	98	99	97	99	98.5
Tension set at 100% %	10	18	30	41	54

(cont...)

5	(cont...table 1	
	Breakdown of ingredients	
	EPDM:	
10	-bonded propylene content, by weight:	35%
	-bonded ethylene content, by weight:	59.5%
	-bonded ENB content, by weight:	5.5%
	-McConey viscosity at 121 °C, ML (1'+4')	65
15	Polypropylene:	
	-fluidity (ASTM-D 1238/L) at 230 °C, applying 2.16 kg:	8.5 g/10'
20	-module of elasticity (ASTM-D 790)	12000 kg/cm ²
	-Rockwell hardness (ASTM-D 785/B)	94° scale R
	Paraffin:	
25	-paraffin oil content, by weight	62%
	-naphthenic oil content, by weight	28%
	-aromatic oil content, by weight	10%
30	Test methods adopted in determining the physical and mechanical properties listed above	
	U.T.S.	
35	Elongation at U.T.S.-	ASTM-D 425/54
	Shore hardness	ASTM 2240/68
	%-cross-linking of EPDM	solubility in xylol at 130 °C
	Tension set	ASTM-D 412

Example 2

The mixing procedure is the same as that utilized in example 1, though employing plastomer-elastomer components with different physical and structural properties -viz,

- 45 -EPDM containing 45% by weight of bonded propylene, 51.5% by weight bonded ethylene, and 3.5% by weight bonded ENB (ethylidene-norbornene);
- polypropylene possessing fluidity of 0.75 g/10' at 230 °C, applying 2.16 kg (ASTM-D 1238/L), modulus of elasticity of 13500 kg/cm² (ASTM-D 790), and scale R Rockwell hardness of 90° (ASTM-D 785/B).

Other ingredients remain the same as in example 1, likewise the ASTM test methods by which physical and mechanical properties are determined.

Table 2 illustrates the composition and the physical and mechanical properties of thermoplastic compounds from tests A, B, C, D, E as envisaged in example 2.

TABLE 2

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	INGREDIENTS	Quantities expressed as parts per 100 parts EPDM					
10		A	B	C	D	E	
	EPDM	100	100	100	100	100	
15	Polypropylene	30	80	110	200	300	
	Paraffin oil	40	60	80	100	120	
	Phenolic resin - resol	12.5	12.5	12.5	13	13	
	Salicylic acid	3.4	3.4	3.4	3.6	3.6	
20	Physical and mechanical properties of compounds measured on specimens punched from injection molded slabs						
25		A	B	C	D	E	
	U.T.S. kg/cm ²	55	70	120	180	195	
30	Elongation at U.T.S. %	350	410	520	540	560	
	Shore hardness A pts	70	78	85	-	-	
	Shore hardness D pts	-	-	-	35	40	
35	Proportion of total EPDM content cross- linked (by weight) %	99	99	98	99	99	
	Tension set at 100% %	7	15	22	35	40	

Example 3

The mixing procedure is the same as that utilized in example 1, though employing plastomer-elastomer components with different physical and structural properties to those of the first two examples: -viz,

45 -EPDM, an oil, mingled at a rate of 23% by weight with an oil of substantially paraffin composition and containing 32 parts bonded propylene per 100 parts of the pure polymer (without oil), 61 parts bonded ethylene per 100 of the pure polymer, and 7 parts bonded ENB (ethylidene-norbornene) per 100 of pure polymer;

50 -polypropylene, a random copolymer consisting of 98% polypropylene and 2% polyethene, by weight, which possesses fluidity of 6 g/10' at 230 °C, applying 2.16 kg (ASTM-D 1298/L), modulus of elasticity of 850 kg/cm² (ASTM-D 790), and Rockwell hardness of 79°, scale R (ASTM-D 256).

Other ingredients remain the same as in examples 1 and 2, likewise the ASTM test methods adopted. Table 3 overleaf illustrates the composition and the physical and mechanical properties of thermoplastic compounds obtained from tests A, B, C, D and E as envisaged in example 3.

TABLE 3

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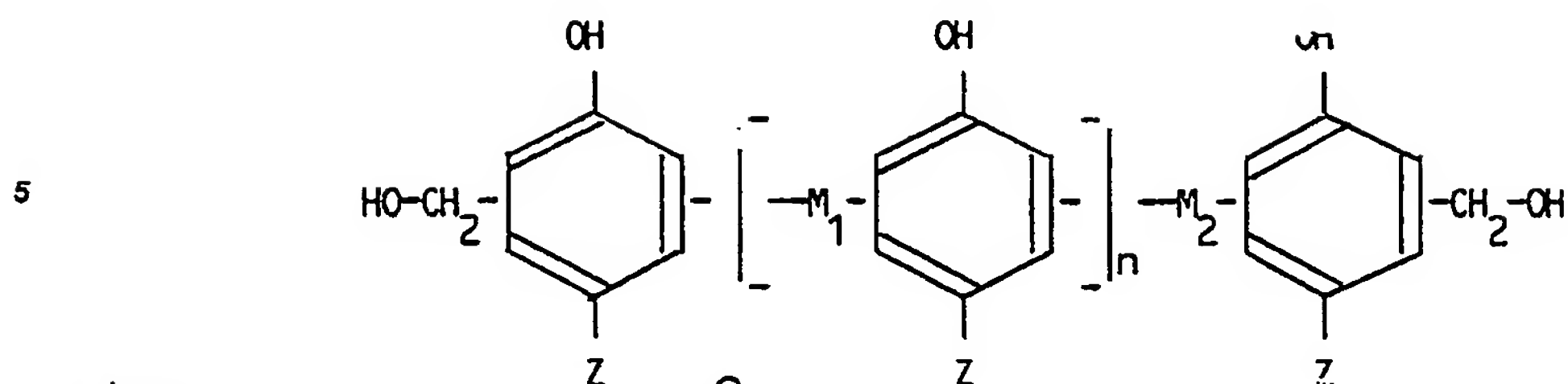
INGREDIENTS	Quantities expressed as parts per 100 parts EPDM				
	A	B	C	D	E
EPDM	130	130	130	130	130
Polypropylene	40	100	150	200	250
Paraffin oil	10	25	50	60	80
Phenolic resin - resol	8	8	8	8.5	9
Salicylic acid	2	2	2	2.2	2.5
Physical and mechanical properties of compounds measured on specimens punched from injection molded slabs					
	A	B	C	D	E
U.T.S. kg/cm^2	60	85	140	185	210
Elongation at U.T.S. %	400	430	480	500	530
Shore hardness A pts	68	81	88	-	-
Shore hardness D pts	-	-	40	50	62
Proportion of total EPDM content cross- linked (by weight) %	95	95	96	92	97
Tension set at 100% %	10	15	18	35	40

Claims

1) A process for the preparation of plastomer-elastomer compounds from EPDM terpolymers and polyolefin resins, wherein the elastomer phase is partly or totally cross-linked, characterized in that the cross-linking agent adopted consists in a non-halogenated phenolic resin together with an aromatic carboxylic acid.

2) Process as in claim 1, wherein the non-halogenated phenolic resin conforms to a general written formula (I):

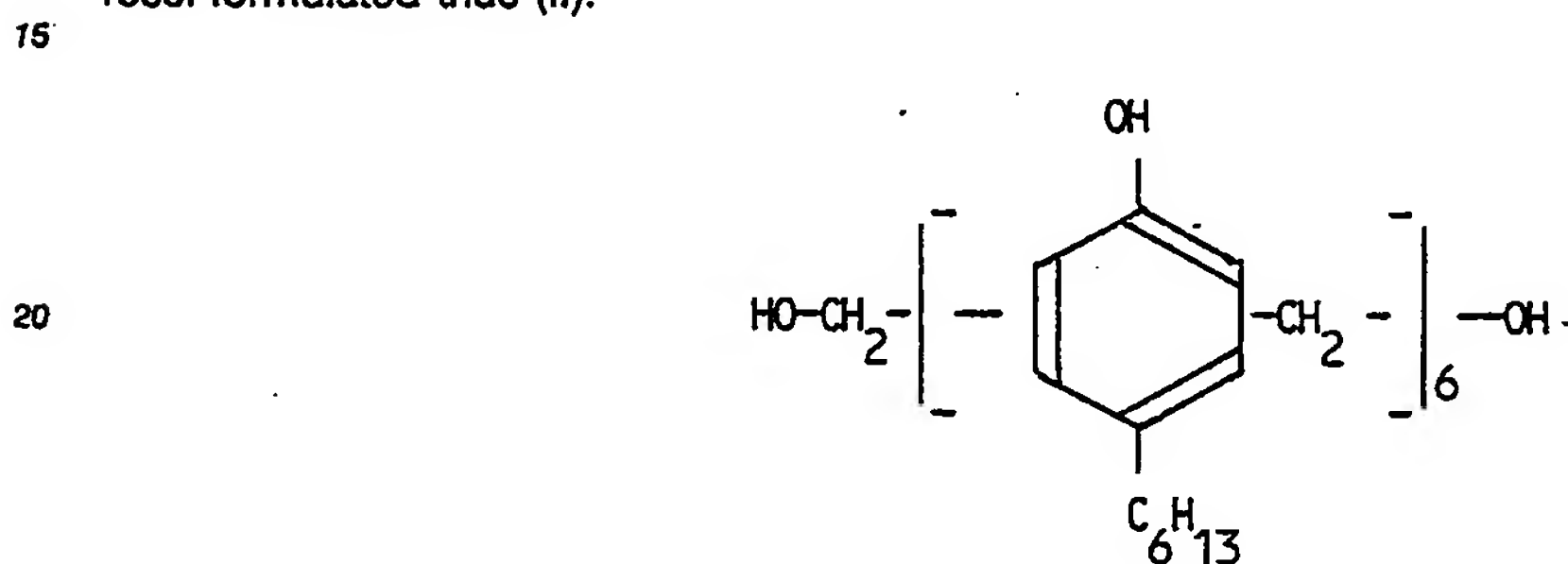
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where

- 10 M₁ and M₂ are radicals -CH₂- or -CH₂-C(=O)-CH₂-, which can be identical or otherwise;
 Z is an alkylenic, aryl or alkyl radical having from 4 to 16 carbon atoms;
 n is an integer between 0 and 6.

3) Process as in claim 1, wherein the non-halogenated phenolic resin is a phenol-formaldehyde type resol formulated thus (II):



4) Process as in claims 1, 2 and 3, wherein the carboxylic acid is salicylic acid.

5) Process as in claim 4, wherein salicylic acid is admixed at a rate of 0.05...12 parts per 100 parts, by weight, of the EPDM elastomer.

6) Process as in claims 1 to 5, wherein the phenolic resin adopted is admixed at a rate of 0.5...15 parts, per 100 parts, by weight, of the EPDM elastomer.

7) Process as in claims 1 to 6, wherein a weight ratio of 0.1...0.8 : 1 is established between salicylic and non-halogenated phenolic resin.

8) An EPDM-polyolefin plastomer-elastomer compound having a partly or totally cross-linked elastomer phase, characterized

in that cross-linking is achieved employing a non-halogenated phenolic resin as in formula I of claim 2, ideally a phenol-formaldehyde type resol as in formula II of claim 3, together with salicylic acid.

9) Plastomer-elastomer compound as in claim 8, wherein the polyolefin is a copolymer obtained by inter-reaction of olefinic monomers such as ethylene, propylene, 1-butene, 1-pentene, 1-hexene, 4-methyl-1-pentene, 3-methyl-1-pentene, 3,3-dimethyl-1-butene 3-methyl-1-hexene and 2,4,4-trimethyl-1-pentene and the like.

10) Plastomer-elastomer compound as in claims 8 and 9, containing 10...90% polyolefin and 90...10% EPDM terpolymer.

11) Plastomer-elastomer compound as in claims 8, 9 and 10, wherein the EPDM terpolymer consists in at least two olefinic monomers and a diene monomer that may or may not be linked to the main polymer chain.

12) Plastomer-elastomer compound as in claims 8 to 11, the olefinic monomers in which are ethylene and/or propylene and/or 1-butene.

13) Plastomer-elastomer compound as in claims 8 to 12, the diene monomer in which is selected from ethylidene-norbornene, 1,4-hexadiene, dicyclopentadiene, 2-methyl-1,4-pentadiene, 1,4,9-decatriene, 1,5-cyclooctadiene, 1-methyl-1,5-cyclooctadiene, 1,4-cyclopentadiene, polybutene, polybutadiene, and their derivatives.

14) Plastomer-elastomer compounds as in claims 8 to 13, prepared by implementation of a process as in claims 1 to 7 and suitable for the manufacture of moulded, extruded, laminated and similar products.